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UAA2016

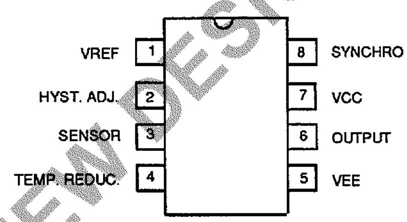
Zero Voltage Switch Power Controller

SILICON MONOLITHIC INTEGRATED CIRCUIT

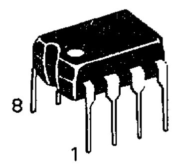
The UAA2016 is designed to drive triacs with the Zero Voltage technique which allows RFI-free power regulation of resistive loads. Operating directly on the AC power line, its main application is the precision regulation of electrical heating systems (panel heaters, irons, etc...).

A built-in digital sawtooth signal permits proportional temperature regulation action over a 1°C band around the set point. For energy saving there is a programmable temperature reduction function and for security a sensor failsafe that inhibits output pulses when the sensor connection is broken. Preset temperature (i.e. defrost) application is also possible. In applications where high hysteresis is needed, its value can be adjusted up to 5°C around set point. All these features come with a very low external component count.

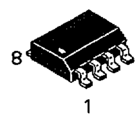
- Zero voltage switch for Triacs, up to 2 kW (MAC212A8).
- Direct AC line operation.
- Proportional regulation of temperature over a 1°C band.
- Programmable temperature reduction.
- Preset temperature (i.e. defrost).
- Sensor failsafe.
- Adjustable hysteresis.
- Low external component count.



PIN ASSIGNMENT



P SUFFIX
PLASTIC PACKAGE
CASE 626-05



D SUFFIX
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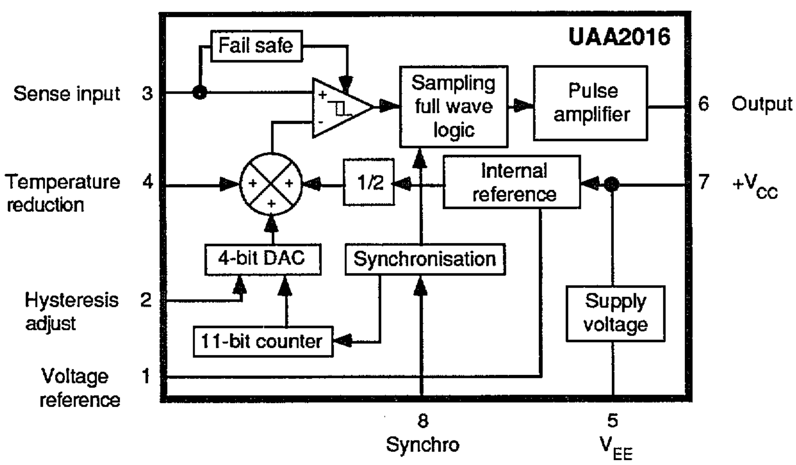
CASE 751-03
SOP-8

BLOCK DIAGRAM



MAXIMUM RATINGS (Voltages referred tp pin 7)

Rating	Symbol	Value	Unit
Supply Current (I pin 5)	I_{CC}	15	mA
Non Repetitive Supply Current (Maximum pulse width = 1 µs)	I_{CCP}	200	mA
AC Synchronization Current	I_{Sync}	3	mA
Maximum Pin Voltages	$V_{Pin\ 2}$ $V_{Pin\ 3}$ $V_{Pin\ 4}$ $V_{Pin\ 6}$	0 ; V_{Ref} 0 ; V_{Ref} 0 ; V_{Ref} 0 ; V_{EE}	Volts Volts Volts Volts
Maximum VREF Current Sink	$I_{Pin\ 1}$	1	mA
Maximum Output Current (Pin 6) (Pulse width < 400 µs)	I_{OM}	150	mA
Power Dissipation	P_D	625	mW
Maximum Thermal Resistance	R_{ThJA}	100	°C/W
Operating Temperature Range	T_A	–20 to +85	°C

NOTES ON ELECTRICAL CHARACTERISTICS (see Table on facing page)

1. Output pulses are centered with respect to zero crossing point. Pulse width is adjusted by the value of R_{Sync}. Refer to application curves.

2. The actual sawtooth period depends on the AC power line frequency. It is exactly 2048 times the corresponding period. For the 50 Hz case it is 40.96 s. For the 60 Hz case it is 34.13 s. This is to comply with the European standard, namely that 2 kW loads cannot be connected or removed from the line more than once every 30 s.

3. 350 mV corresponds to 5°C temperature reduction. This is tested at probe using internal test pad. Smaller temperature reduction can be obtained by adding an external resistor between Pin 4 and V_{CC}. Refer to application curves.

4. 350 mV corresponds to a hysteresis of 5°C. This is tested at probe using internal test pad. Smaller additional hysteresis can be obtained by adding an external resistor between Pin 2 and V_{CC}. Refer to application curves.

5. Parameter guaranteed but not tested. Worst case 10 mV corresponds to 0.15°C shift on set point.

6. Measured at probe by internal test pad. 70 mV corresponds to 1°C. Note that the proportional band is independent of the NTC value.

7. At very low temperature the NTC resistor increases quickly. This can cause the sensor input voltage to reach the failsafe threshold, thus inhibiting output pulses: refer to application schematics. The corresponding temperature is the limit at which the circuit works in the typical application. By setting this threshold at 0.05 V_{Ref}, the NTC value can increase up to 20 times its nominal value, thus the application works below –20°C.

ELECTRICAL CHARACTERISTICS (T_A = 25°C, V_{EE} = –7V, Voltages referred to pin 7 unless otherwise noted)

Characteristics	Symbol	Min	Typ	Max	Unit
Supply Current (Pins 6 and 8 not connected) (T_A = –20 to +85°C)	I_{CC}		0.9	1.5	mA
Stabilized Supply Voltage (Pin 5) (I_{CC} = 2 mA)	V_{EE}	–10	–9	–8	Volts
Reference Voltage (Pin 1)	V_{Ref}	–6.5	–5.5	–4.5	Volts
Output Pulse Current (Fig. 1) (R_{Out} = 60 W V_{EE} = –8 V) (T_A = –20 to +85°C)	I_{Out}	90	100	130	mA
Output Leakage Current (V_{out} = 0 V)	I_{OL}			10	µA
Output Pulse Width (Note 1) T_A = –20 to +85°C (Mains = 220 V_{RMS}, R_{Sync} = 220 kΩ)	T_p	50		100	µS
Comparator Offset (Note 5)	V_{Off}	–10		+10	mV
Sensor Input Bias Current	I_{IB}			0.1	µA
Sawtooth Period (Note 2)	T_S		40.96		S
Sawtooth Amplitude (Note 6)	A_S	50	70	90	mV
Temperature Reduction Voltage (Note 3) (Pin 4 connected to V_{CC})	V_{TR}	280	350	420	mV
Internal Hysteresis Voltage (Pin 2 not connected)	V_{IH}		10		mV
Additional Hysteresis (Note 4) (Pin 2 connected to V_{CC})	V_H	280	350	420	mV
Failsafe Threshold (Note 7) T_A = –20 to +85°C	V_{FSth}	180		300	mV

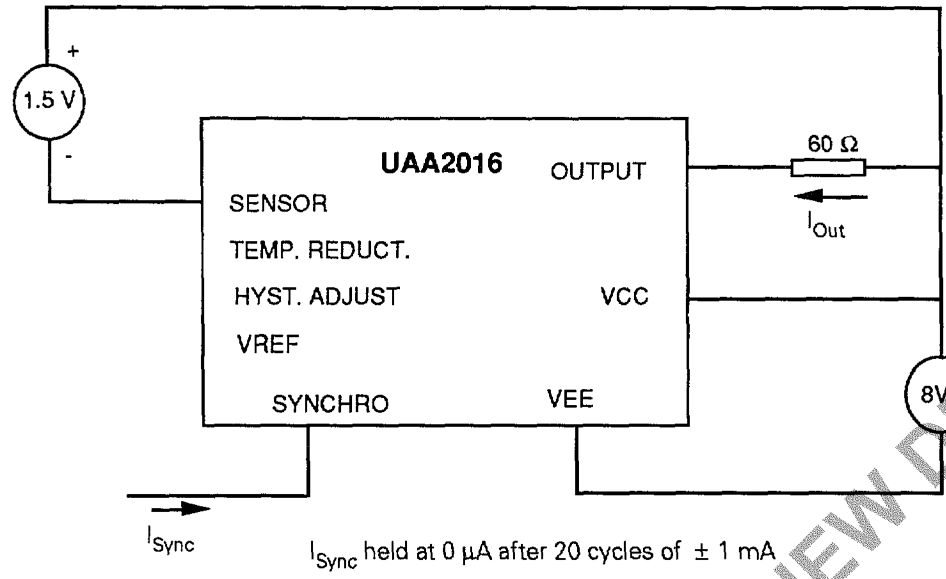


Figure 1. I_{out} test schematic

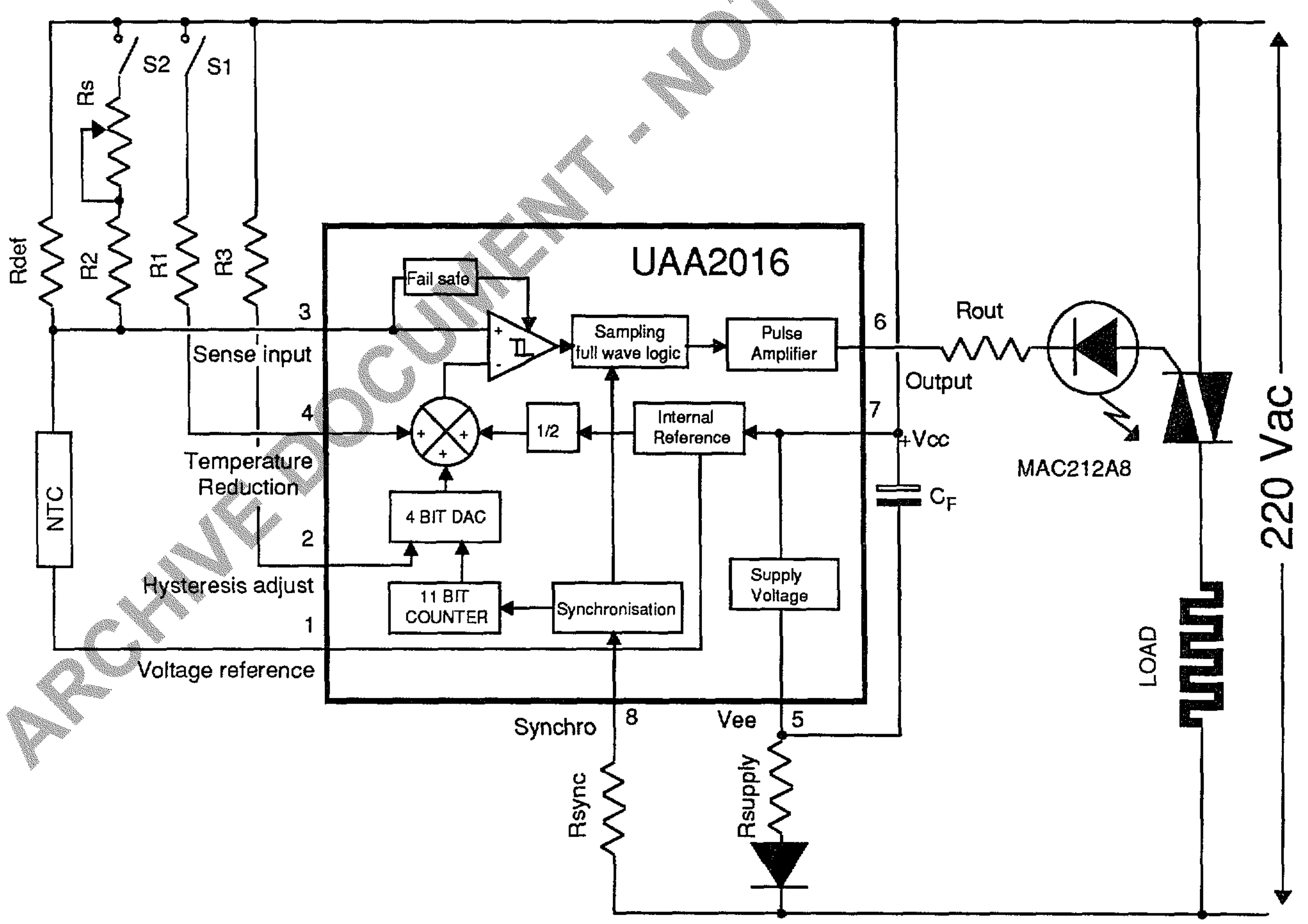


Figure 2. Application schematic

APPLICATION NOTES (For simplicity, the LED in series with R_{Out} is omitted in the following calculations)

1. Triac choice and R_{Out} determination

   Depending on the power in the load, choose the Triac that has the lowest peak gate trigger current. This will limit the output current of the UAA2016 and thus its power consumption. Use Figure 5 to determine R_{Out} according to the triac max gate current I_{gt} and the application low temperature limit. For a 2 kW load at 220 V_{RMS}, a good triac choice is the Motorola MAC212A8. Its maximum peak gate trigger current at 25°C is 50 mA.

   For an application to work down to –20°C, R_{Out} should be 60 Ω.

   It is assumed that

   $I_{gt}(T) = I_{gt}(25°C) \times \exp(-T/125)$ with T in °C,

   which applies to the MAC212A8.

2. Output pulse width, R_{Sync}

   The pulse width T_p is determined by the Triac I_{Hold}, I_{Latch} together with the load value and working conditions (frequency and voltage):

   - Given the RMS AC voltage and the load power, the load value is: $R_L = V^2_{RMS} / POWER$
   - The load current is then:
     $I_{Load} = (V_{RMS} \times \sqrt{2} \times \sin(2\pi ft) - V_{TM}) / R_L$

     where V_{TM} is the maximum on state voltage of the triac, f is the line frequency.
   - Set $I_{Load} = I_{Latch}$ for $t = T_p/2$ to calculate T_p.

   Figures 7 and 8 give the value of T_p which corresponds to the higher of the values of I_{Hold} and I_{Latch}, assuming that V_{TM} = 1.6 V. Figure 9 gives the R_{Sync} that produces the corresponding T_p.

3. R_{Supply} and filter capacitor

   With the output current and the pulse width determined as above, use Figures 10 and 11 to determine R_{Supply}, assuming that the sinking current at V_{Ref} pin (including NTC bridge current) is less than 0.5 mA. Then use Figures 12 and 13 to determine the filter capacitor C_F according to the ripple desired on supply voltage. The maximum ripple allowed is 1V.

4. The temperature reduction is determined by R_1 (see Figures 14 and 15).

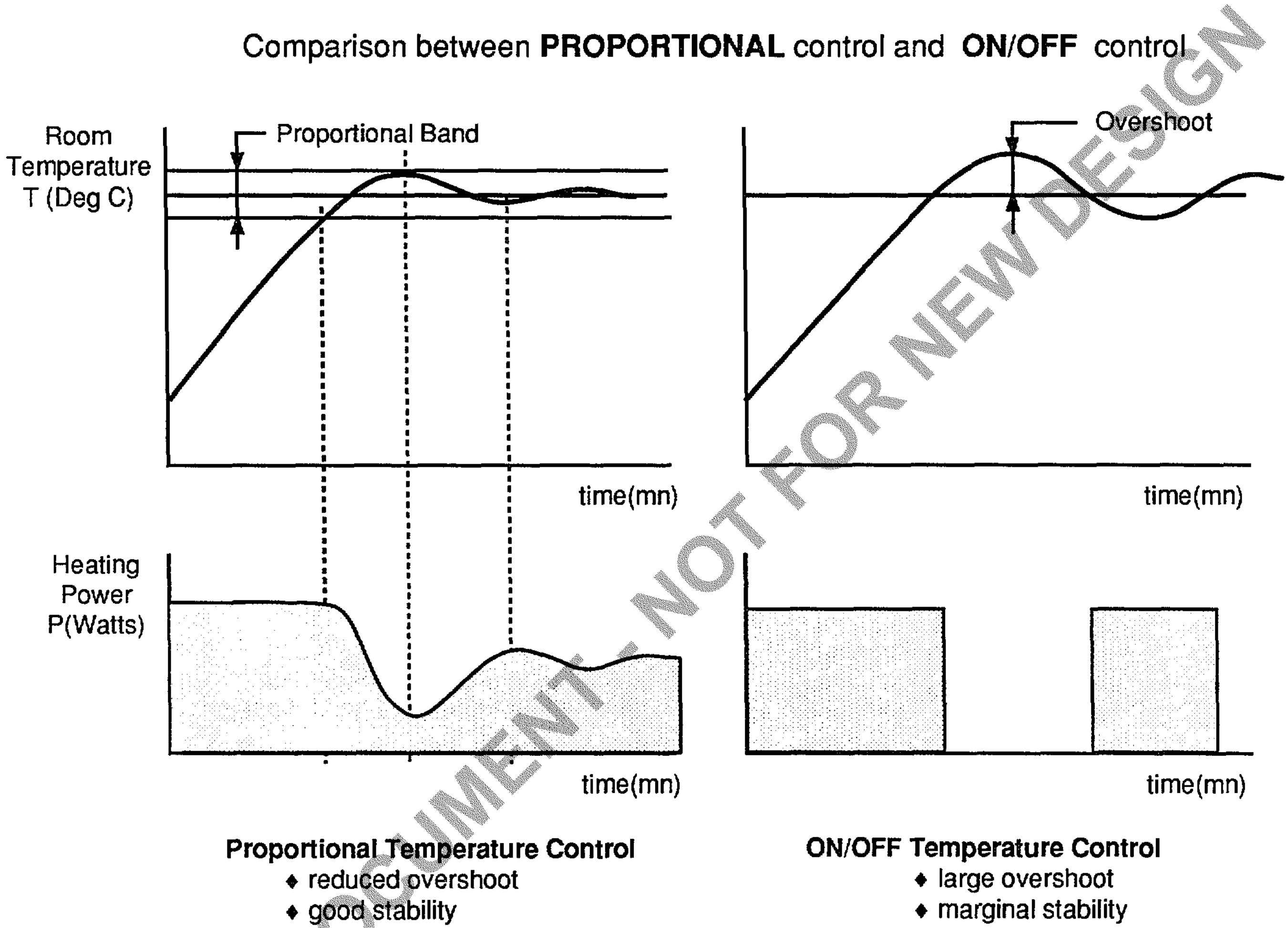
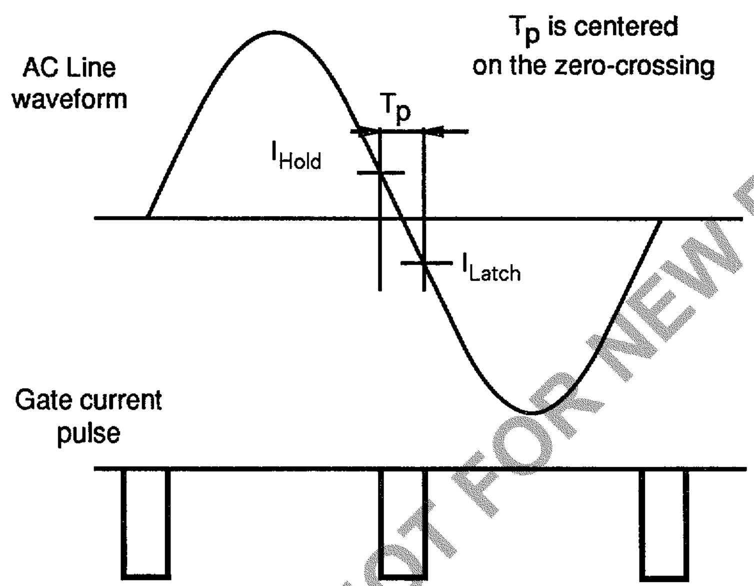


Figure 3. Proportional control



$$T_p = \frac{14 \times R_{Sync} + 7 \times 10^5}{V_{RMS} \times \sqrt{2} \times \pi f} \quad (\mu S)$$

f	:	AC line frequency (Hz)
V_{RMS}	:	AC line RMS voltage (V)
R_{Sync}	:	Synchronisation resistor (Ω)

Figure 4. Zero voltage technique

CIRCUIT FUNCTIONAL DESCRIPTION

POWER SUPPLY – PIN 5 AND PIN 7

The application uses a current source supplied by a single high voltage rectifier in series with a power dropping resistor. An integrated shunt regulator delivers a V_{EE} voltage of –8.6 V with respect to Pin 7. The current used by the total regulating system can be shared in four functional blocks: IC supply, sensing bridge, Triac gate firing pulses and zener current. The integrated zener, as in any shunt regulator, absorbs the excess supply current. The 50 Hz pulsed supply current is smoothed by the large value capacitor connected between Pins 5 and 7.

TEMPERATURE SENSING – PIN 3

The actual temperature is sensed by a negative temperature coefficent element connected in a resistor divider fashion. This 2 element network is connected between the ground terminal Pin 7 and the reference voltage –5.5 V available on Pin 1. The resulting voltage – a function of the measured temperature – is applied to Pin 3 and internally compared to a control voltage whose value depends on several elements: Sawtooth, Temperature Reduction and Hysteresis Adjust. (See Application Notes.)

COMPARATOR

When the positive input (Pin 3) receives a voltage greater than the internal reference value, the comparator allows the triggering logic to deliver pulses to the Triac gate. To improve the noise immunity the comparator has an adjustable hysteresis. The external resistor R3 connected to Pin 2 sets the hysteresis level. Setting Pin 2 open makes a 10 mV hysteresis level, corresponding to 0.15°C. Maximum hysteresis is obtained by connecting Pin 2 to V_{CC}. In that case the level is set at 5°C. This configuration can be useful for low temperature inertia systems.

TEMPERATURE REDUCTION

For energy saving, a remotely programmable temperature reduction is available on Pin 4. The choice of resistor R1 connected between Pin 4 and V_{CC} sets the temperature reduction level.

SAWTOOTH GENERATOR

In order to comply with European norms the ON/OFF period on the load must exceed 30 seconds. This is achieved by an internal digital sawtooth which performs the proportional regulation without any additional component. The sawtooth signal is added to the reference applied to the comparator negative input. Figure 3 shows the regulation improvement using the proportional band action.

NOISE IMMUNITY

The noisy environment requires good immunity. Both the voltage reference and the comparator hysteresis minimize the noise effect on the comparator input. In addition the effective Triac triggering is enabled every $^1/_3$ sec.

FAIL SAFE

Output pulses are inhibited by the "fail safe" circuit if the comparator input voltage exceeds the specified threshold voltage. This would occur if the temperature sensor circuit is open.

SAMPLING FULL WAVE LOGIC

Two consecutive zero-crossing trigger pulses are generated at every positive mains half-cycle. This ensures that the number of delivered pulses is even in every case. The pulse length is selectable by R_{Sync} connected on Pin 8. The pulse is centered on the zero-crossing mains waveform.

PULSE AMPLIFIER

The pulse amplifier circuit sinks current pulses from Pin 6 to V_{EE}. The minimum amplitude is 70 mA. The Triac is then triggered in quadrants II and III. The effective output current amplitude is given by the external resistor R_{Out}. Eventually a LED can be inserted in series with the Triac gate (see Figure 2).

Figure 5. Output Resistor versus Triac Gate Current

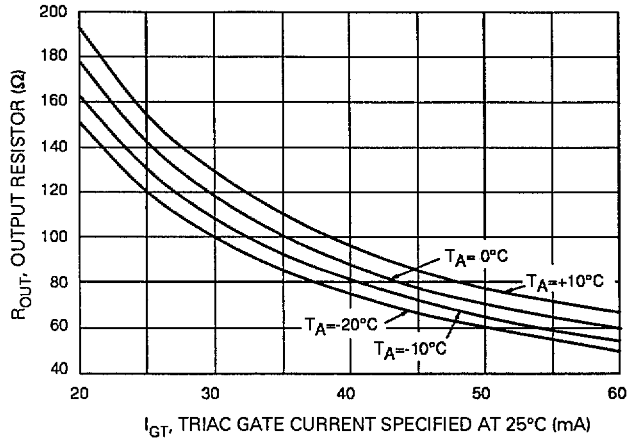


Figure 6. Minimum Output Current versus Output Resistor

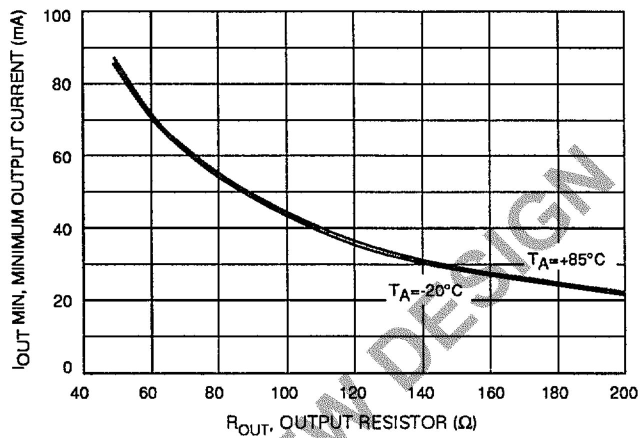


Figure 7. Output Pulse Width versus Maximum Triac Latch Current

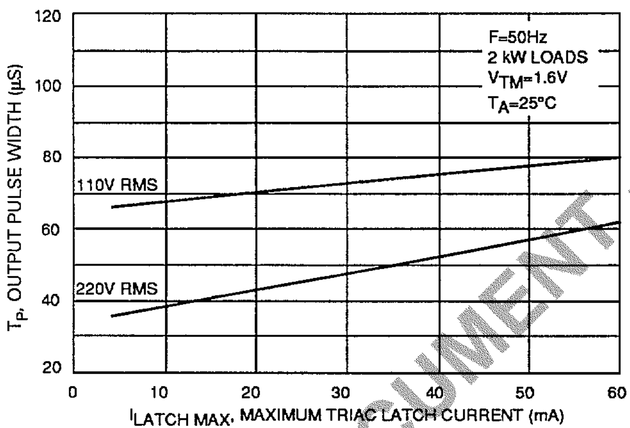


Figure 8. Output Pulse Width versus Maximum Triac Latch Current

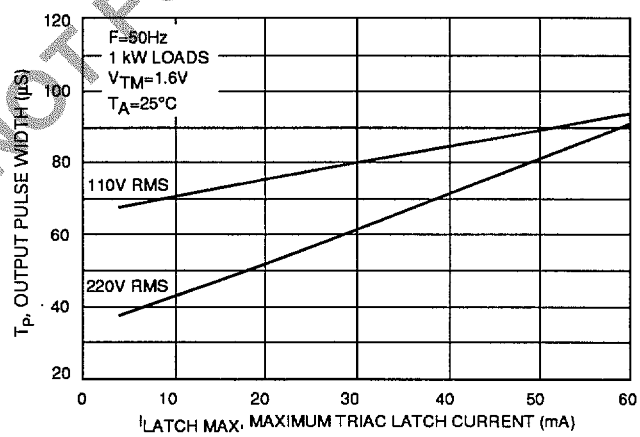


Figure 9. Synchronisation Resistor versus Output Pulse Width

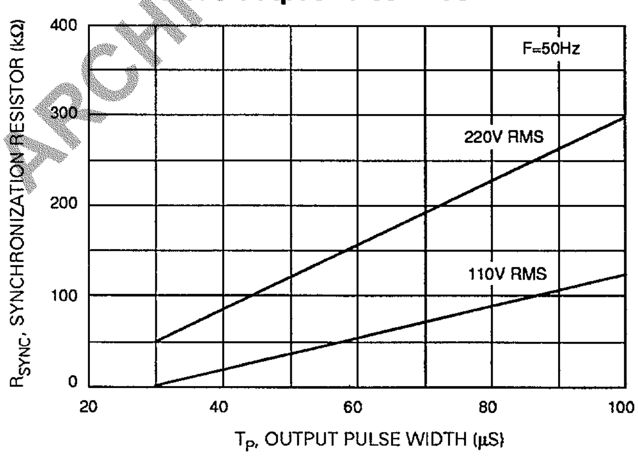


Figure 10. Maximum Supply Resistor versus Output Current

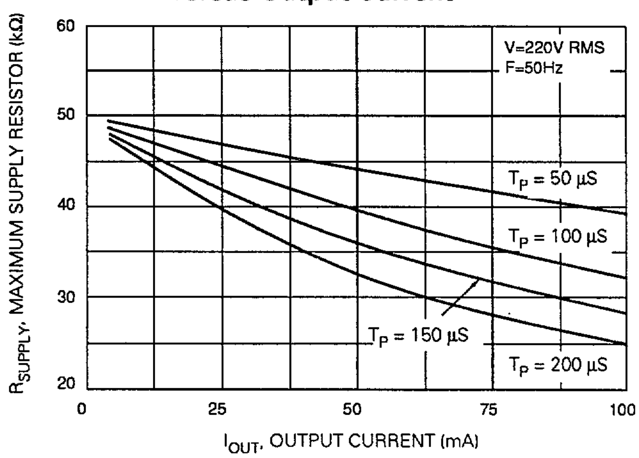


Figure 11. MaximumSupply Resistor versus Output Current

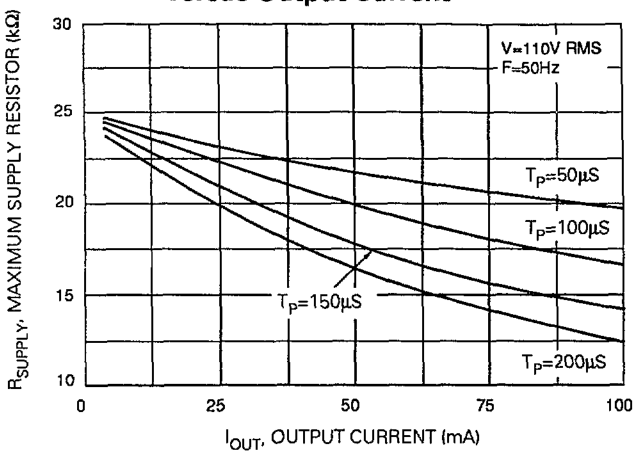


Figure 12. Minimum Filter Capacitor versus Output Current

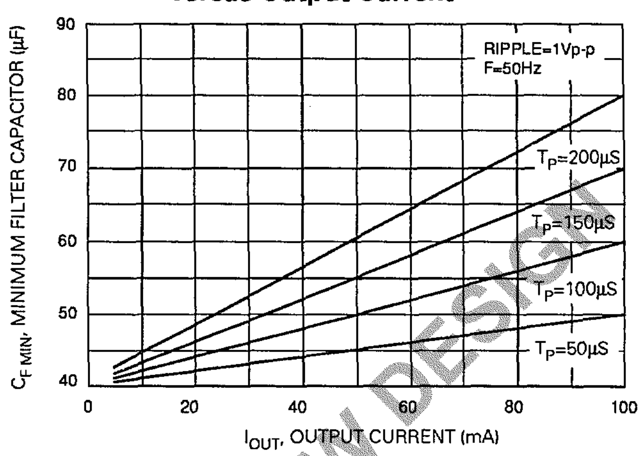


Figure 13. Minimum Filter Capacitor versus Output Current

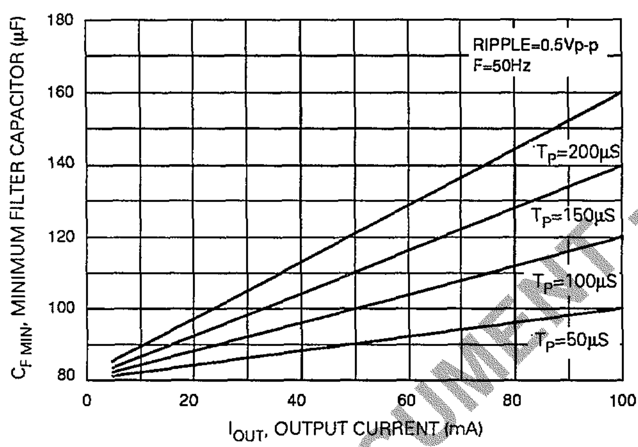


Figure 14. Temperature Reduction versus R_1

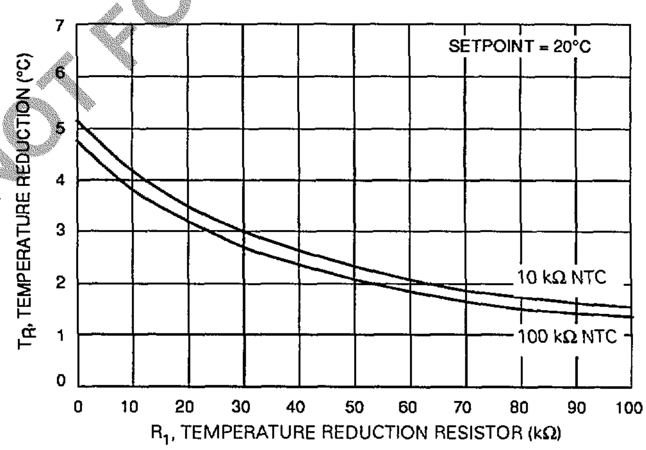


Figure 15. Temperature Reduction versus Temperature Setpoint

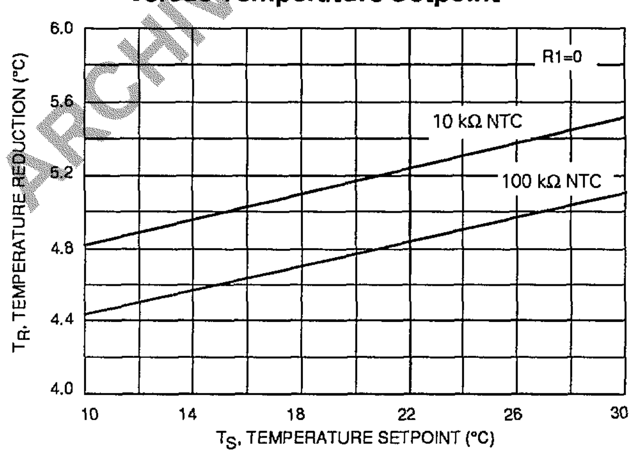


Figure 16. R_{DEF} versus Preset Temperature

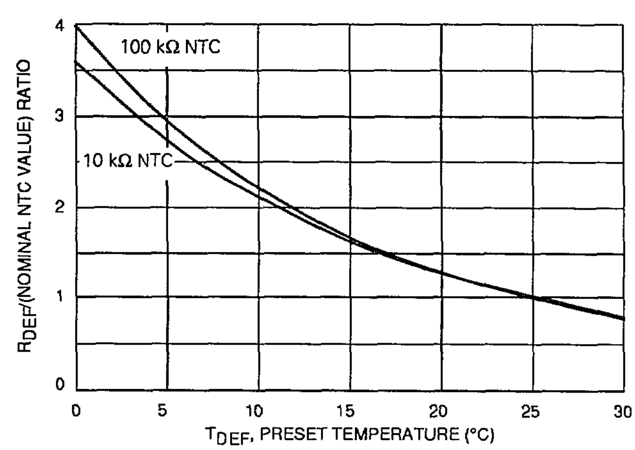


Figure 17. $R_S + R_2$ versus Preset Setpoint

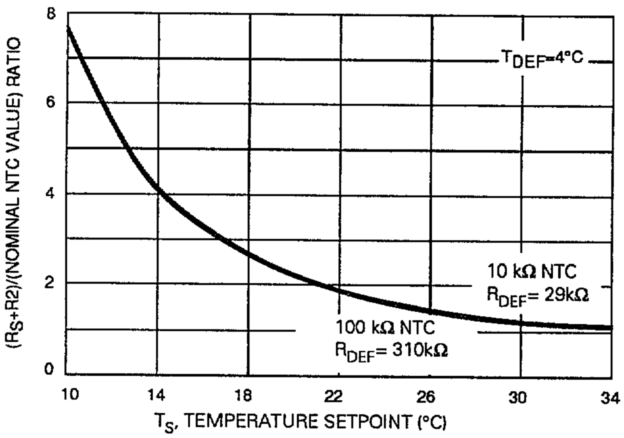
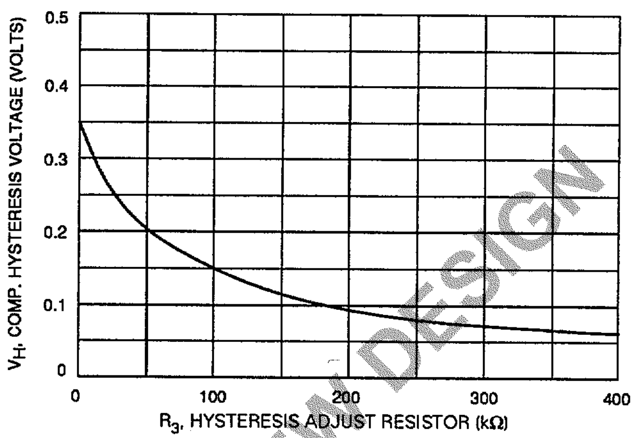


Figure 18. Comparator Hysteresis versus R_3



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Printed in Great Britain by Tavistock Press (Bedford) Ltd. 4500 1/91, PO.1356